

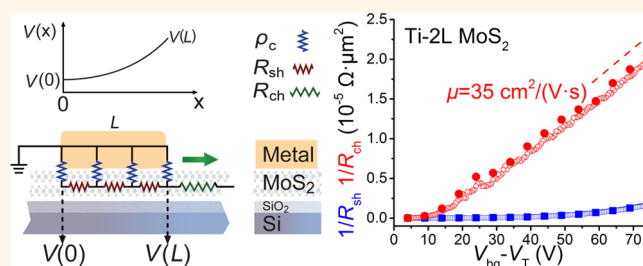
# Study on the Resistance Distribution at the Contact between Molybdenum Disulfide and Metals

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**ABSTRACT** Contact resistance hinders the high performance of electrical devices, especially devices based on two-dimensional (2D) materials, such as graphene and transition metal dichalcogenide. To engineer contact resistance, understanding the resistance distribution and carrier transport behavior at the contact area is essential. Here, we developed a method that can be used to obtain some key parameters of contact, such as transfer length ( $L_t$ ), sheet resistance of the 2D materials beneath the contacting metal ( $R_{sh}$ ), and contact resistivity between the 2D materials and the metal electrode ( $\rho_c$ ). Using our method, we studied the contacts between molybdenum disulfide ( $\text{MoS}_2$ ) and metals, such as titanium and gold, in bilayer and few-layered  $\text{MoS}_2$  devices. Especially, we found that  $R_{sh}$  is obviously larger than the sheet resistance of the same 2D materials in the channel ( $R_{ch}$ ) in all the devices we studied. With the increasing of the back-gate voltage,  $L_t$  increases and  $R_{sh}$ ,  $\rho_c$ ,  $R_{ch}$ , and the contact resistance  $R_c$  decrease in all the devices we studied. Our results are helpful for understanding the metal– $\text{MoS}_2$  contact and improving the performances of  $\text{MoS}_2$  devices.



**KEYWORDS:**  $\text{MoS}_2$  · FET · contact resistance · two-dimensional materials · transfer length

Along with the scaling down of electronic devices, contact resistance is playing a more and more important role in circuit resistance and hinders the high performance of circuits.<sup>1</sup> After decades of engineering on the metal–Si contact, the contact resistance of silicon-based devices has been lowered to an acceptable level.<sup>2</sup> Two-dimensional (2D) materials, such as graphene and transition metal dichalcogenides, have fascinating properties in some aspects and show great potential in future electronic devices.<sup>3–5</sup> Field effect transistors (FETs) based on molybdenum disulfide ( $\text{MoS}_2$ ) have been demonstrated to have several impressive characteristics, such as an ON/OFF current ratio as high as  $10^8$ , reasonable electron mobility up to hundreds of  $\text{cm}^2/(\text{V}\cdot\text{s})$ , a subthreshold swing approaching the theoretical limit of 60 mV/dec at room temperature, and atomically thin layered structure, suppressing short-channel effects.<sup>4,6–8</sup> However, the metal– $\text{MoS}_2$  contact resistance ( $R_c$ ) is up to  $5 \text{ k}\Omega\cdot\mu\text{m}$  to  $1 \text{ M}\Omega\cdot\mu\text{m}$ , which is more than 30 times larger than that of the metal–Si contact.<sup>8,9</sup>

Such a high contact resistance blocks further performance optimization regardless of the efforts on enhancing the carrier mobility or scaling the channel length.<sup>10,11</sup>

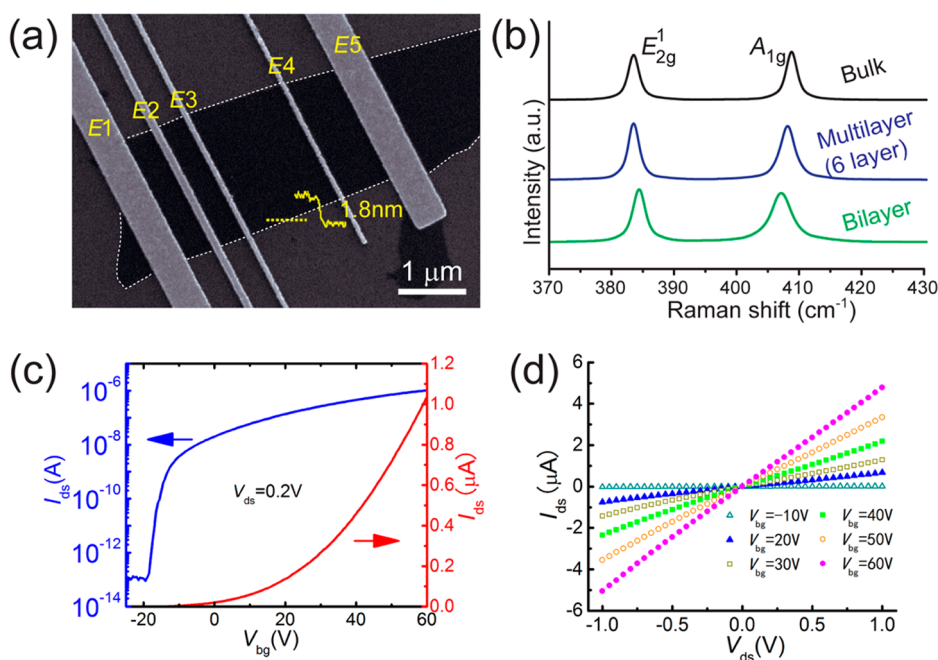
So far, the origin of large metal– $\text{MoS}_2$  contact resistance is unclear. Several possible explanations have been proposed: the wide contact tunnel barrier at the interface blocking electron tunneling between the metal and  $\text{MoS}_2$ , the large layer-to-layer resistance between  $\text{MoS}_2$  layers, and the Schottky barrier related to the work function of the contacting metal.<sup>7,9,12–15</sup> Using a contacting metal with a low work function, molecular doping and a thin interlayer “insulation” barrier have been reported to lower the effective Schottky barrier.<sup>7,16–18</sup> However, to the best of our knowledge, acceptable contact resistance for high-performance devices has not been reported, yet there is much more work to do to pave the way to the utilization of  $\text{MoS}_2$  as an electronic material. To further engineer metal– $\text{MoS}_2$  contact, a deep understanding of the resistance distribution and carrier transport behavior at the contact area is urgently needed.

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**Figure 1.** (a) SEM image of the Ti–2L MoS<sub>2</sub> device. The MoS<sub>2</sub> sheet has darker contrast compared to the substrate and is outlined by the white dotted line. The metal electrodes were marked from E1 to E5. A height difference between the MoS<sub>2</sub> sheet and the substrate obtained by AFM is marked. (b) Raman spectrum of a bulk MoS<sub>2</sub>, the 2L MoS<sub>2</sub> in (a), and a 6L MoS<sub>2</sub>. Transfer (c) and output (d) characteristics of the 2L MoS<sub>2</sub> FET, using E1, E5, and the substrate as the source, drain, and back-gate electrodes.

Here we discuss metal–MoS<sub>2</sub> contact particularly. Different from the generally used four-probe method and transfer length method to obtain contact resistance, we develop a method to study the detailed resistance distribution at contact area. Through experimental measurements, we obtain some key parameters of the contacts between MoS<sub>2</sub> and metals, such as titanium (Ti) and gold (Au). Our results are helpful for understanding and reducing the contact resistance of metal–MoS<sub>2</sub> contact.

## RESULTS AND DISCUSSION

As shown in Figure 1a, five electrodes were fabricated to contact the same individual MoS<sub>2</sub> sheet on a SiO<sub>2</sub>/Si substrate, marked as E1, E2, E3, E4, and E5. The MoS<sub>2</sub> sheet shown in Figure 1a has two layers (2L), confirmed by atomic force microscopy (AFM) study and Raman spectrum (Figure 1b).<sup>19</sup> The electrode materials of the 2L MoS<sub>2</sub> device shown in Figure 1a are 5 nm Ti/65 nm Au. The transfer and output characteristics of this device were measured using E1, E5, and the Si substrate as the source, drain, and back-gate electrodes. As shown in Figure 1c and d, the results agree well with those in the literature.<sup>4</sup> The threshold voltage ( $V_T$ ) is  $-14$  V, extracted using the second derivative of  $\ln(I_{ds})$  method.<sup>20</sup> The  $I_{ds}$ – $V_{ds}$  curves are symmetric and linear within the measuring range. The electrical characteristic of the device is observed to be stable, and repeated measurements provide reproducible results. In addition to this bilayer MoS<sub>2</sub> (2L MoS<sub>2</sub>) device with Ti–2L MoS<sub>2</sub> contact, seven devices with similar structure based on multilayer MoS<sub>2</sub> (ML MoS<sub>2</sub>)

with Ti–ML MoS<sub>2</sub> contact (four devices) and Au–ML MoS<sub>2</sub> contact (three devices) were also fabricated and successfully studied. The data measured from a Ti–6L MoS<sub>2</sub> device and a Au–6L MoS<sub>2</sub> device are shown in Supporting Information I. We choose Ti and Au as examples of contact metals because Ti has a lower work function, while Au has a higher work function.

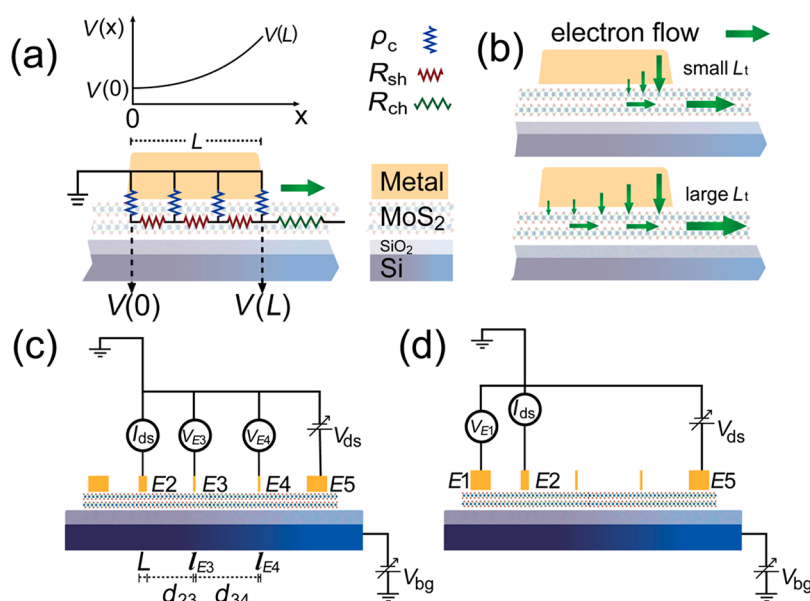
We consider the metal–MoS<sub>2</sub> contact in MoS<sub>2</sub> FETs as that shown in Figure 2a.  $\rho_c$  is the contact resistivity of the metal–MoS<sub>2</sub> contact.  $R_{sh}$  and  $R_{ch}$  are the sheet resistance of the MoS<sub>2</sub> sheet beneath the contact and in the channel, respectively. Note that in the conventional transfer length method  $R_{sh}$  and  $R_{ch}$  are treated as being identical based on the assumptions that the metal–semiconductor contact is a completely “diffusive” one and the sheet resistance under the metal is not affected significantly by the metal. However, these assumptions, especially the second one, may not be valid in the contact between 2D materials and metals.<sup>21</sup> Here, for the first time to the best of our knowledge, we treat  $R_{sh}$  and  $R_{ch}$  as being different in the metal–MoS<sub>2</sub> contact.

When a metal electrode is grounded, the potential of the electrode is 0. According to Ohm’s law and Kirchhoff’s law, we have

$$dV(x)/dx = I(x)R_{sh}/W \quad (1)$$

$$dI(x)/dx = WV(x)/\rho_c \quad (2)$$

where  $V(x)$  is the potential of the MoS<sub>2</sub> sheet beneath the metal,  $I(x)$  is the current in the MoS<sub>2</sub> sheet along the  $x$  direction, and  $W$  is the width of the contact. Here,  $\rho_c$  and  $R_{sh}$  are assumed to be independent of  $V(x)$  at small



**Figure 2.** (a) Schematic diagram showing the contact resistance model we used. (b) Schematic diagrams of the current distribution with small (upper diagram) and large (lower diagram)  $L_t$ . (c) Schematic circuit diagram for measuring  $V_{E3}$ ,  $V_{E4}$ , and  $I_{ds}$ . (d) Schematic circuit diagram for measuring  $V_{E1}$  and  $I_{ds}$ .

$V_{ds}$ ; this assumption is confirmed to be reasonable by our results obtained below that  $R_c$  is independent of  $V_{ds}$ . Note that for metal–ML MoS<sub>2</sub> contact,  $\rho_c$  is an effective contact resistivity rather than the absolute resistivity of the metal–MoS<sub>2</sub> interface, because carriers transport through several MoS<sub>2</sub> layers as well as the metal–MoS<sub>2</sub> interface along the sheet normal direction.<sup>9</sup> The coupled equations have simple solutions considering the boundary condition that  $I(x)$  is zero at  $x = 0$ . For an electrode with length  $L$  (as shown in Figure 2a), we have

$$V(L) = V(0) \cosh(L\sqrt{R_{sh}/\rho_c}) \quad (3)$$

$$V(L)/I(L) = \sqrt{R_{sh}\rho_c} \coth(L\sqrt{R_{sh}/\rho_c})/W \quad (4)$$

where  $V(0)$  is the potential of the MoS<sub>2</sub> sheet at  $x = 0$ ,  $V(L)$  is the potential of the MoS<sub>2</sub> sheet at  $x = L$ , and  $I(L)$  is the current of the MoS<sub>2</sub> sheet at  $x = L$ . From another point of view, as the metal electrode is grounded,  $V(L)$  equals the voltage drop on the whole contact, and  $I(L)$  is the current going out of the contact and flowing through the channel between the source and drain. Therefore,  $I(L) = I_{ds}$  and the contact resistance is

$$R_c = V(L)/I_{ds} \quad (5)$$

Transfer length,

$$L_t = \sqrt{\rho_c/R_{sh}} \quad (6)$$

is a parameter that describes the effective conductive length of the contact near the channel. As shown in Figure 2b, for small  $L_t$ , current crowds around the edge of the contact, while for large  $L_t$ , more contact area is involved in the current transport.<sup>22,23</sup>

The resistance distribution at the contact area of  $E2$  is studied through the measurements using the circuits

schematically shown in Figure 2c and d. In the measurements,  $E2$  was grounded and used as the source,  $E5$  was used as the drain, the Si substrate was used as the back gate, and  $E1$ ,  $E3$ , and  $E4$  were used as voltage probes. One type of measurement (noted as M1) was performed as follows: at a fixed source–drain voltage  $V_{ds} = 0.2$  V, the back-gate voltage ( $V_{bg}$ ) was swept with a step of 0.5 V in a range, such as from  $-10$  V to  $+60$  V, electrical parameters  $I_{ds}$ ,  $V_{E3}$ , and  $V_{E4}$  were measured as shown in Figure 2c, and  $I_{ds}$  and  $V_{E1}$  were measured as shown in Figure 2d. Besides such measurement, we also performed another type of measurement (noted as M2) as follows: at a fixed  $V_{bg}$ , we swept  $V_{ds}$  from  $-1$  V to  $1$  V and measured  $I_{ds}$ ,  $V_{E1}$ ,  $V_{E3}$ , and  $V_{E4}$  as shown in Figure 2c and d, and then changed  $V_{bg}$  step by step with each step being 5 V and measured the above parameters again. The results obtained from M1 and M2 are consistent (as shown together in Figures 3–5), indicating our results are reliable. When the length of  $E2$  ( $L$ , varies from 104 to 130 nm among different devices in the present work) is comparable to the transfer length  $L_t$  of the contact,  $V(0)$  equals the measured voltage of electrode  $E1$ ,  $V_{E1}$ . Otherwise, if  $L \gg L_t$ ,  $V(0)$  drops close to 0 and could not be measured. That is the reason that we elaborately designed the length of electrode  $E2$ . More detailed discussion on the accuracy and reliability of the above measurements is given in Supporting Information II.

With the data obtained from the above measurements, the resistance distribution of  $E2$  can be obtained, but the calculation is not simple. Normally, the effect of voltage probes is neglected. However, neglecting the effect of  $E3$  and  $E4$  may cause a large error in the present case, because the length of the voltage probes,  $E3$  and  $E4$ , is comparable to the transfer length

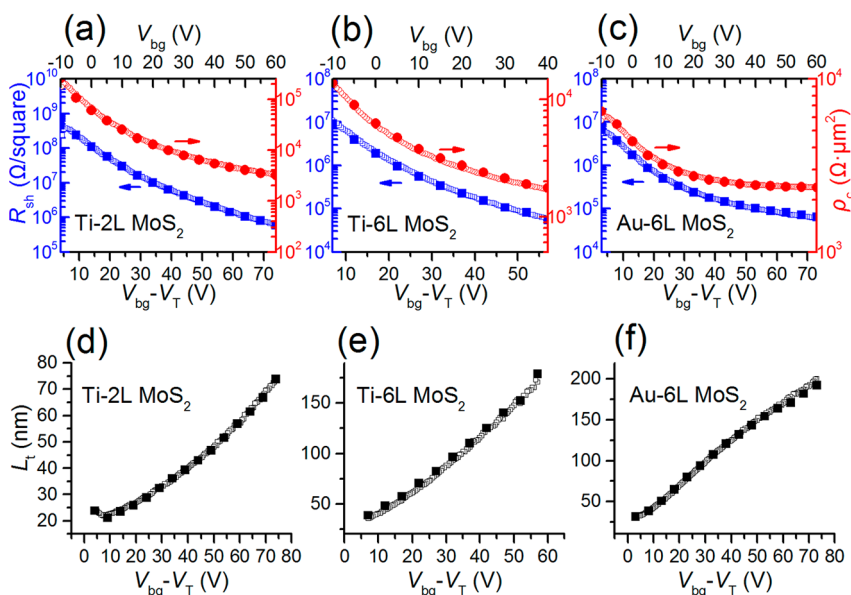


Figure 3. Change of  $R_{sh}$  and  $\rho_c$  as a function of  $V_{bg}$  for the Ti–2L MoS<sub>2</sub> contact (a), the Ti–6L MoS<sub>2</sub> contact (b), and the Au–6L MoS<sub>2</sub> contact (c). Change of  $L_t$  as a function of  $V_{bg}$  for the Ti–2L MoS<sub>2</sub> contact (d), the Ti–6L MoS<sub>2</sub> contact (e), and the Au–6L MoS<sub>2</sub> contact (f). In these figures, the hollow marks were obtained through M1; the solid marks were obtained through M2.

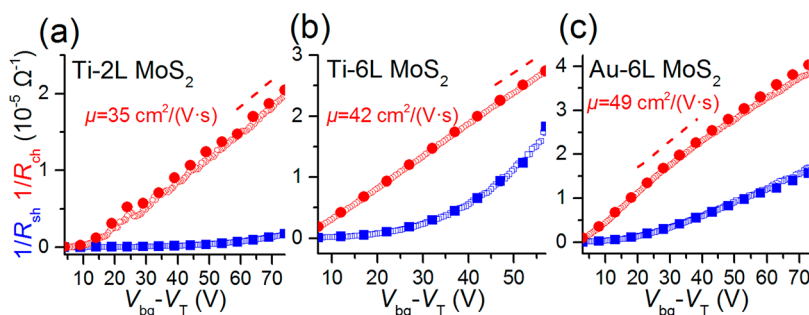


Figure 4. Comparison of  $1/R_{ch}$  (red spheres) and  $1/R_{sh}$  (blue squares) of the Ti–2L MoS<sub>2</sub> device (a), the Ti–6L MoS<sub>2</sub> device (b), and the Au–6L MoS<sub>2</sub> device (c). In these figures, the hollow marks were obtained through M1; the solid marks were obtained through M2.

$L_t$ , as confirmed later. In such a case, current may go into the metal and flow back to the MoS<sub>2</sub> across the contact area of the voltage probes during our measurements (shown in Supporting Information III, Figure S4). Therefore, we considered the effect of  $E_3$  and  $E_4$  during our calculations. Assuming  $R_{sh}$  and  $\rho_c$  are the same for all the contacts, considering the boundary condition that  $I(x) = I_{ds}$  on both the left and the right sides of a voltage probe with length  $l$ , and taking into account that the potential of  $E_3$  and  $E_4$  is not zero, the voltage drop from one side to the other side of a voltage probe,  $\Delta V(l)$ , is

$$\Delta V(l) = 2I_{ds}\sqrt{R_{sh}\rho_c} \tanh\left(\frac{l}{2}\sqrt{R_{sh}/\rho_c}\right)/W \quad (7)$$

The detailed process to derive this equation is given in Supporting Information III. Also,

$$V_{E3} - V(L) = \Delta V(I_{E3})/2 + I_{ds}R_{ch}d_{23}/W \quad (8)$$

$$V_{E4} - V_{E3} = \Delta V(I_{E3})/2 + \Delta V(I_{E4})/2 + I_{ds}R_{ch}d_{34}/W \quad (9)$$

where  $\Delta V(I_{E3})$  and  $\Delta V(I_{E4})$  are the voltage drop across  $E_3$  and  $E_4$ , and  $l_{E3}$  and  $l_{E4}$  are the length of  $E_3$  and  $E_4$ ,

respectively. We can further simplify the equations as follows. From eqs 3 and 4, we obtain

$$V(0) \cosh(L\sqrt{R_{sh}/\rho_c}) = I_{ds}\sqrt{R_{sh}\rho_c} \coth(L\sqrt{R_{sh}/\rho_c})/W \quad (10)$$

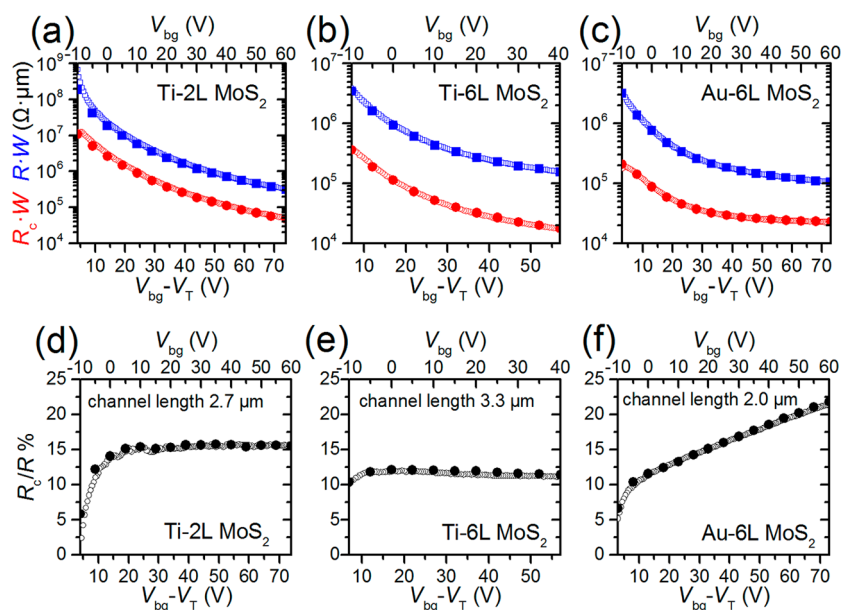
From eqs 3, 7, and 8, we obtain

$$\begin{aligned} V_{E3} - V(0) \cosh(L\sqrt{R_{sh}/\rho_c}) \\ = \frac{I_{ds}}{W} \left[ \sqrt{R_{sh}\rho_c} \tanh\left(\frac{l_{E3}}{2}\sqrt{R_{sh}/\rho_c}\right) + R_{ch}d_{23} \right] \end{aligned} \quad (11)$$

From eqs 7 and 9, we obtain

$$\begin{aligned} V_{E4} - V_{E3} = \frac{I_{ds}}{W} \left[ \sqrt{R_{sh}\rho_c} \tanh\left(\frac{l_{E3}}{2}\sqrt{R_{sh}/\rho_c}\right) \right. \\ \left. + \sqrt{R_{sh}\rho_c} \tanh\left(\frac{l_{E4}}{2}\sqrt{R_{sh}/\rho_c}\right) + R_{ch}d_{34} \right] \end{aligned} \quad (12)$$

Using eqs 10–12, knowing the geometric parameters of the devices measured by scanning electron microscopy (SEM) and the measured  $I_{ds}$ ,  $V_{E1}$ ,  $V_{E3}$ , and  $V_{E4}$ , we can numerically calculate  $R_{sh}$ ,  $\rho_c$ , and  $R_{ch}$  through iteration.



**Figure 5.** Contact resistance  $R_c$  of E2 and the whole device resistance  $R$  of the Ti–2L MoS<sub>2</sub> device (a), the Ti–6L MoS<sub>2</sub> device (b), and the Au–6L MoS<sub>2</sub> device (c). Proportion of contact resistance  $R_c$  in the whole resistance  $R$  of the Ti–2L MoS<sub>2</sub> device (d), the Ti–6L MoS<sub>2</sub> device (e), and the Au–6L MoS<sub>2</sub> device (f). In these figures, the hollow marks were obtained through M1; the solid marks were obtained through M2.

The contact resistance  $R_c$  and the transfer length  $L_t$  can then be obtained using eqs 5 and 6.

Figure 3a–c show  $R_{sh}$  and  $\rho_c$  we obtained at different gate voltage in three typical devices, with Ti–2L MoS<sub>2</sub>, Ti–6L MoS<sub>2</sub>, and Au–6L MoS<sub>2</sub> contacts, respectively. It can be seen that both  $R_{sh}$  and  $\rho_c$  drop severely with increasing  $V_{bg}$  in all three contacts, being consistent with previous reports<sup>14</sup> as well as the expectation considering the accumulation of electrons in the MoS<sub>2</sub> layer at large  $V_{bg}$ ,  $R_{sh}$  drops more severely than  $\rho_c$  as  $V_{bg} - V_T$  increases in all three types of contacts. We observed that both  $R_{sh}$  and  $\rho_c$  are more sensitive to the number of layers than to the contacting metals. It is observed that both  $R_{sh}$  and  $\rho_c$  in the Ti–2L MoS<sub>2</sub> contact are obviously larger than those in the Ti–6L MoS<sub>2</sub> and Au–6L MoS<sub>2</sub> contacts at the same  $V_{bg} - V_T$ . One of the reasons might be attributed to the rise of the conduction band bottom in the band structure as the layer number of MoS<sub>2</sub> decreases.<sup>24</sup> In the same  $V_{bg} - V_T$  range, both  $R_{sh}$  and  $\rho_c$  drop more severely in the Ti–2L MoS<sub>2</sub> contact than in the Ti–6L MoS<sub>2</sub> and Au–6L MoS<sub>2</sub> contacts. Comparing the contacts between 6L MoS<sub>2</sub> and different metals (Ti and Au),  $R_{sh}$  does not differ a lot, but  $\rho_c$  is obviously different. The smallest  $\rho_c$  we obtained (which is 1.8 k $\Omega \cdot \mu\text{m}^2$  in Ti–6L MoS<sub>2</sub> when  $V_{bg} - V_T = 57$  V) is obviously larger than that in the best metal–graphene contact reported in the literature.<sup>25</sup>

We observed that  $L_t$  increases with the gate voltage in most of the cases in all the contacts, as shown in Figure 3d–f. This is because  $R_{sh}$  drops more severely than  $\rho_c$  as  $V_{bg} - V_T$  increases (shown in Figure 3a–c). For the Ti–2L MoS<sub>2</sub> contact,  $L_t$  is only 24 nm when

$V_{bg} - V_T = 4$  V, indicating that a rather limited area of the contact is involved in electron transmission.  $L_t$  increased from 24 to 74 nm as  $V_{bg} - V_T$  increases from 4 V to 74 V, indicating a relief of current crowding and the broadening of the effective current path; more carriers go a longer distance along the contact in the MoS<sub>2</sub> layers before transferring into the metal or reverse at larger  $V_{bg}$ .  $L_t$  of the Ti–6L MoS<sub>2</sub> contact is larger than that of the Ti–2L MoS<sub>2</sub> contact at the same gate voltage and increases from 39 nm to 179 nm as  $V_{bg} - V_T$  increases from 7 V to 57 V.  $L_t$  of the Au–6L MoS<sub>2</sub> contact is roughly the same as that of the Ti–6L MoS<sub>2</sub> contact at the same gate voltage and increases from 31 nm to 192 nm as  $V_{bg} - V_T$  increases from 3 V to 73 V. The fact that we obtained consistent results from eight devices (shown in Supporting Information IV, Figure S5) supports the reliability of our method. Previous work on a CVD monolayer MoS<sub>2</sub> sheet has also found that current flows not only at the edge of the metal contact but also in the metal contact area with a large contact length.<sup>14</sup> However,  $L_t$  is larger than 600 nm in that report and decreases with the back-gate voltage. As we treat  $R_{sh}$  and  $R_{ch}$  as being different, the present  $R_{sh}$  and  $L_t$  are not exactly the same as those in the literature.

In Figure 4, the sheet conductance of the MoS<sub>2</sub> sheet beneath the metal electrode ( $1/R_{sh}$ ) is compared with that of the channel ( $1/R_{ch}$ ) for three typical devices. In all the devices we studied,  $1/R_{sh}$  is obviously smaller than  $1/R_{ch}$  in the whole voltage range we studied (the difference at low gate voltage can be seen clearly when the data are presented in the logarithmic coordinates in Supporting Information V, Figure S6), indicating that

the property of the atomically thin MoS<sub>2</sub> sheets has been changed after contacting the metal electrode. For the 2L MoS<sub>2</sub> device,  $1/R_{\text{sh}}$  is more than 1 order of magnitude smaller than  $1/R_{\text{ch}}$  in almost the whole  $V_{\text{bg}}$  range we measured. While for the 6L MoS<sub>2</sub> device, the difference between  $1/R_{\text{sh}}$  and  $1/R_{\text{ch}}$  decreased at high  $V_{\text{bg}}$ . In previous studies on the transfer length  $L_{\text{t}}$  at the contact between 2D materials and metals,  $R_{\text{sh}}$  and  $R_{\text{ch}}$  are normally treated as being the same.<sup>23,26</sup> However, our present results show that  $R_{\text{sh}}$  and  $R_{\text{ch}}$  of thin MoS<sub>2</sub> are different, especially when the thickness of the materials is atomically thin.

The conductivity degeneration of the materials beneath the contacting metal might be due to the following reasons. Impurities and defects might be introduced to the MoS<sub>2</sub> sheets at the contact area when metal electrodes were fabricated. Defects have been reported to lower the contact resistivity between the metal and MoS<sub>2</sub>,<sup>27,28</sup> however, they may increase carrier scattering and increase  $R_{\text{sh}}$ . As both  $\rho_{\text{c}}$  and  $R_{\text{sh}}$  contribute to the contact resistance, the defects may need to be engineered to obtain the smallest  $R_{\text{c}}$ . Strain might be introduced to the MoS<sub>2</sub> sheets at the contact area by the contacting metals and change the electrical properties of the MoS<sub>2</sub> sheets, and inhomogeneous strain could introduce additional carrier scattering.<sup>29–31</sup> The metal with a large work function might reduce the electron density in the MoS<sub>2</sub> layers.<sup>7</sup> The metal could also change the dielectric environment of the MoS<sub>2</sub> sheets and partially screen the effect of the back-gate voltage. Due to the large charge screening length of MoS<sub>2</sub> ( $\lambda_{\text{MoS}_2} = 7 \text{ nm}$ ),<sup>9</sup> the screening of the metal could have a significant effect on the ability of the back-gate voltage to modulate the electron density in the MoS<sub>2</sub> sheet contacting the metal. Raman peak shifts have been observed on MoS<sub>2</sub> after it was deposited by thin Pd, Au, and Ag films.<sup>29</sup> We also observed Raman peak shifts caused by Ti and Au thin films as shown in Supporting Information VI, Figure S7, supporting that the property of the atomically thin MoS<sub>2</sub> sheets has been changed after contacting the metal. More work is under way to understand these Raman peak shifts.

Carrier mobility  $\mu$  was also extracted from the data shown in Figure 4 considering  $d(1/R_{\text{ch}}) = \mu C_{\text{ox}} d(V_{\text{bg}} - V_{\text{T}})$ , where  $C_{\text{ox}}$  is the capacity per unit area of the 300 nm silicon oxide. Note that the present extracted mobility is the property of the channel on the substrate, while the field effect mobility normally extracted from the transfer curve of a device is affected by the existence of contact resistance. The carrier mobility extracted from the present devices has a reasonable value.

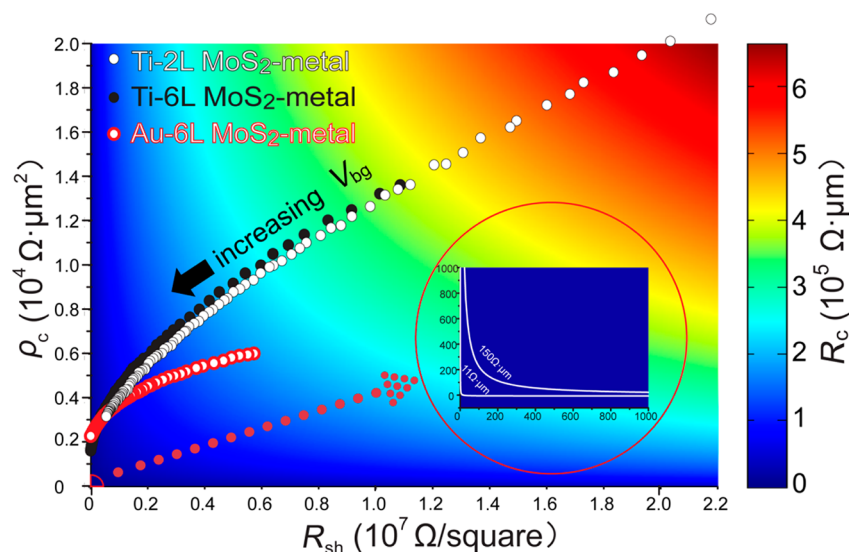
The contact resistance  $R_{\text{c}}$  of E2 in the three typical devices is compared with the total resistance  $R = V_{\text{ds}}/I_{\text{ds}}$  in Figure 5. For a better comparison among different devices, normalized  $R_{\text{c}}$ ,  $R_{\text{c}}W$ , is presented in Figure 5a–c. Both  $R_{\text{c}}$  and  $R$  decrease as  $V_{\text{bg}}$  increases in all three devices, similar to  $R_{\text{ch}}$  (as shown in Figure 4),

indicating the gate voltage modulates the contact as well as the channel in the ON state we studied. Previous work on a CVD monolayer MoS<sub>2</sub> sheet reported that the contact resistance ( $R_{\text{c}}$ ) decreases by more than 2 orders as  $V_{\text{bg}}$  increased about 100 V.<sup>14</sup> Here, we observed that  $R_{\text{c}}$  in the Ti–2L MoS<sub>2</sub> device decreases by more than 2 orders of magnitude when  $V_{\text{bg}}$  increases by about 70 V. However,  $R_{\text{c}}$  in the Ti–6L MoS<sub>2</sub> device decreases by less than 1.5 orders of magnitude as  $V_{\text{bg}}$  increases by about 50 V, and  $R_{\text{c}}$  in the Au–6L MoS<sub>2</sub> device decreases by about 1 order of magnitude as  $V_{\text{bg}}$  increases by about 70 V.

Although  $R_{\text{sh}}$  is obviously larger than  $R_{\text{ch}}$ , as the channel length in the present devices is at least 1 order of magnitude longer than  $L_{\text{t}}$ ,  $R_{\text{c}}$  is still a small part in the total resistance  $R$ , being less than 17% of  $R$  in the Ti–2L MoS<sub>2</sub> device, about 10–12% of  $R$  in the Ti–6L MoS<sub>2</sub> device, and less than 23% in the Au–6L MoS<sub>2</sub> device in the whole  $V_{\text{bg}}$  range we studied (as shown in Figure 5d–f). The fraction of  $R_{\text{c}}$  in  $R$  in the Ti–MoS<sub>2</sub> devices increases with gate voltages at low  $V_{\text{bg}} - V_{\text{T}}$  and then remains roughly the same when  $V_{\text{bg}} - V_{\text{T}} > 20 \text{ V}$  in the 2L MoS<sub>2</sub> device and  $V_{\text{bg}} - V_{\text{T}} > 15 \text{ V}$  in the 6L MoS<sub>2</sub> device. In the Au–6L MoS<sub>2</sub> device, the fraction of  $R_{\text{c}}$  in  $R$  increases rapidly with gate voltage at low  $V_{\text{bg}} - V_{\text{T}}$  and then increases slowly but linearly with gate voltage when  $V_{\text{bg}} - V_{\text{T}} > 10 \text{ V}$ . In all these devices, if the channel length decreases to a couple hundred nanometers, the fraction of  $R_{\text{c}}$  in  $R$  could increase to be the main part of  $R$ , as has been shown in previous reports.<sup>10</sup> Therefore, it is crucial to reduce  $R_{\text{c}}$  to achieve high performance in short-channel devices.

Until now we obtain a resistance distribution using thin electrodes with their length comparable to the transfer length. This method takes advantage of the potential distribution of the 2D materials beneath a thin electrode and measures the electrical characteristics of the contact directly. The method is also applicable for other metal–2D material contact with large  $L_{\text{t}}$ .

On the basis of the present results, we discuss some key strategies to reduce metal–MoS<sub>2</sub> contact resistance. First, the length of the contact electrodes must be larger than  $L_{\text{t}}$ . For a contact with  $L \gg L_{\text{t}}$ , eq 4 degenerates to  $R_{\text{c}} = (R_{\text{sh}}\rho_{\text{c}})^{1/2}/W$ . Thus, reducing  $\rho_{\text{c}}$  and  $R_{\text{sh}}$  are the two key ways to reduce  $R_{\text{c}}$ . Most of the previous work studying metal–MoS<sub>2</sub> contact has focused on reducing  $\rho_{\text{c}}$ , such as engineering the work function and band alignment and processing annealing.<sup>7,8</sup> Our results show that  $R_{\text{sh}}$  also plays an important part in constituting contact resistance, and reducing  $R_{\text{sh}}$  is equally important in engineering the contact resistance. Several methods have been used to reduce  $R_{\text{c}}$ , probably through reducing  $R_{\text{sh}}$ . A gentle metal deposition process and cleaning method might reduce the defects and impurities in MoS<sub>2</sub> introduced in the device fabrication process. As  $R_{\text{sh}}$  of the metal–ML MoS<sub>2</sub> contact is less affected than the metal–2L MoS<sub>2</sub> contact, ML MoS<sub>2</sub>



**Figure 6.** Color map of  $R_c$  versus  $\rho_c$  and  $R_{sh}$ . The target contour lines for  $R_c = 150 \Omega \cdot \mu\text{m}$  (metal–Si contact) and  $R_c = 11 \Omega \cdot \mu\text{m}$  (metal–graphene contact) are enlarged and shown within the circle.

is more preferable to make low contact resistance devices. Engineering the dielectric environment may also improve the contact. Recently, an interlayer between MoS<sub>2</sub> layers and a metal has also been demonstrated to improve contact effectively.<sup>17,32</sup> Such an interlayer might also protect the MoS<sub>2</sub> sheets from being damaged in the device fabrication process. As shown in the color map of  $R_c$  in Figure 6, increasing  $V_{bg}$  could effectively reduce both  $\rho_c$  and  $R_{sh}$ . The three types of metal–MoS<sub>2</sub> contacts follow a similar trend with increasing  $V_{bg}$ . However, there is still a long way toward the target of  $R_c = 150 \Omega \cdot \mu\text{m}$  (the value of the metal–Si contact) as well as  $R_c = 11 \Omega \cdot \mu\text{m}$  (the best value of the metal–graphene contact).

## CONCLUSIONS

In summary, we developed a method to obtain a resistance distribution using narrow electrodes with length comparable to the transfer length. The method is also applicable for other metal–2D material contact with large  $L_t$ . Through this method, we studied the detailed resistance distribution in metal–MoS<sub>2</sub> contacts in the ON-state devices. For the first time to the best of our knowledge, we treat the sheet resistance of the MoS<sub>2</sub> sheet beneath the electrode ( $R_{sh}$ ) and that in

the channel ( $R_{ch}$ ) as being different in the metal–MoS<sub>2</sub> contact. Similar to that in the literature, both  $R_{sh}$  and  $R_{ch}$  decrease with increasing gate voltage. However,  $R_{sh}$  is obviously larger than  $R_{ch}$  in all the metal–MoS<sub>2</sub> contacts (such as Ti–2L MoS<sub>2</sub>, Ti–6L MoS<sub>2</sub>, and Au–6L MoS<sub>2</sub> contacts) in the whole gate voltage range we studied, indicating the MoS<sub>2</sub> in the contact area has been changed by contacting the metal electrode, while the amount of difference between  $R_{sh}$  and  $R_{ch}$  is different in various metal–MoS<sub>2</sub> contacts and at different gate voltage.

Both  $\rho_c$  and  $R_{sh}$  decrease with increasing gate voltage, but  $R_{sh}$  drops more severely, so that  $L_t$  increases with increasing  $V_{bg} - V_T$ , indicating a relief of current crowding and the broadening of the effective current path at large  $V_{bg}$ .  $L_t$  of the metal–6L MoS<sub>2</sub> contact is larger than that of the Ti–2L MoS<sub>2</sub> contact at the same  $V_{bg}$ . In the Ti–2L MoS<sub>2</sub> contact,  $L_t$  is only 24 nm when  $V_{bg} - V_T = 4$  V. The largest  $L_t$  we obtained is 218 nm for the Au–5L MoS<sub>2</sub> contact when  $V_{bg} - V_T$  is 72 V.

As the channel length of the present devices is much longer than  $L_t$ , the contact resistance  $R_c$  is less than 23% of the total resistance of the circuit  $R$  in all the devices we studied. However,  $R_c$  could be the main part of  $R$  in short-channel devices.

## METHODS

**Device Fabrication.** MoS<sub>2</sub> sheets were exfoliated onto a heavily doped silicon wafer covered by 300 nm of silicon dioxide. Rectangular sheets with homogeneous contrast were selected under an optical microscope.<sup>33</sup> Two-layered photoresist (copolymer plus PMMA) and electron beam lithography were used to define the electrodes. A metal film of 5 nm Ti/65 nm Au was deposited to form the Ti–MoS<sub>2</sub> contact, and 0.3 nm Ti/70 nm Au was deposited to form the Au–MoS<sub>2</sub> contact by an electron beam evaporator. The length of  $E_2$  was

elaborately designed to be comparable with the transfer length in our experiment. After lift-off in acetone, the wafer was immediately transferred into a vacuum chamber with four probes for electrical characterization with a Keithley 4200 semiconductor characterization system.

**Characterization.** AFM and Raman spectra were used to characterize the thickness and layer number of the MoS<sub>2</sub> sheets.<sup>19,24</sup> A laser with a 488 nm wavelength was used for the Raman spectrum study. The geometric parameters of the devices, including  $W$ ,  $L$ ,  $d_{23}$ ,  $d_{34}$ ,  $l_{E3}$ , and  $l_{E4}$ , were all measured by SEM. The parameters of the three typical devices are listed in Table 1.

TABLE 1. Geometric Parameters and  $V_T$  of the Three Typical Devices

metal	no. of MoS <sub>2</sub> layers	electrode length (nm)					distance between electrodes ( $\mu\text{m}$ )		width ( $\mu\text{m}$ )	threshold voltage (V)
		E1	E2	E3	E4	E5	$d_{23}$	$d_{34}$	$W$	$V_T$
Ti	2	490	117	65	53	490	0.44	1.5	1.9	-14
Ti	6	500	112	65	50	500	0.45	2	2.4	-17
Au	6	510	115	112	111	510	0.44	0.99	2.5	-13

Once the devices had been fabricated, the electrical measurements were performed immediately using the circuits schematically shown in Figure 2c and d. The gate voltage range was chosen so that the devices were in the ON state.

**Conflict of Interest:** The authors declare no competing financial interest.

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**Supporting Information Available:** SEM images and electrical characteristics of the Ti-6L MoS<sub>2</sub> device and the Au-6L MoS<sub>2</sub> device, analysis on the reliability of the electrical measurements, evaluation of the effect of the voltage probes E3 and E4,  $I_c$  of eight metal-MoS<sub>2</sub> contacts, comparison of  $1/R_{ch}$  and  $1/R_{sh}$  in logarithmic coordinates, Raman spectroscopy study of MoS<sub>2</sub> sheets before and after metal deposition. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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